

Background Information

The present invention relates to a magnetic sensor system, in particular for sensing the  
5 motion of elements moved in a linear or rotary manner, according to the generic  
features of the main claim.

It is known per se that sensors that are sensitive to magnetic fields are used in many  
applications where contactless detection of motion is desired. The motion can be rotary  
or linear. A distinction must be made here between two fundamentally different  
10 measurement principles. In one case, one or more magnetic dipoles are mounted, as  
the active elements, on the element to be detected, and the motion is determined  
directly via the magnetic field, which changes with respect to time, at the point where  
the sensor is located. In contrast, with passive transmitter elements, which are made of  
a soft-magnetic material, the magnetic field is produced by a working magnet that is  
15 permanently connected with the sensor. The sensor measures the change in the  
magnetic field of the working magnet caused by the motion of the transmitter elements.

In addition to Hall technology, known per se, for measuring magnetic fields, "XMR"  
technologies, i.e., magnetoresistive measurement principles, are also finding increasing  
use, as an alternative, with passive transmitter elements in automotive applications. It  
20 should be noted that, unlike Hall sensors, XMR sensors detect the "in-plane" component  
of the magnetic field in the sensor element. For this purpose, previously common XMR  
sensors use a working magnet, the field of which must be adjusted such that the offset  
at the location of the sensitive element is zero, or a "backbias" field will be produced that  
defines the working point of the sensor.

25 For example, a concept is described in DE 101 28 135 A1 with which a hard-magnetic  
layer is deposited in the vicinity of, i.e., in particular on and/or under, a magnetoresistive  
layer stack. This hard-magnetic layer is then coupled – primarily via its stray field – with  
the magnetoresistive layers, thereby producing a "bias" magnetic field which acts as the

magnetic field offset, so that, even when an external magnetic field superimposed on the internal magnetic field is varied even slightly, an easily measured and relatively great change in the actual measured value is obtainable, the measured value being detected as a change in resistance in the layer stack.

5 The sensors described above are often utilized in a "gradiometer" system in a manner known per se to measure rotational speed. This means that two branches of a Wheatstone bridge are separated by a specified distance, so that a homogenous magnetic field does not induce a bridge signal. In contrast, a variation of the magnetic field in the region of the predetermined distance produces a bridge signal. The sensor  
10 therefore only measures the signal from a magnetic rotor, the distance between the pairs of poles of which approximately corresponds to the predetermined gradiometer separation.

Unlike the use of XMR elements, which perform absolute measurements, the application of the gradiometer principle in a magnetoresistive XMR measurement bridge  
15 results in a reduction of the sensitivity of the sensors to homogeneous interference fields. An alignment of the magnets used previously, which was carried out so that the offset can be eliminated at both locations of the sensor elements of the gradiometer system, cannot be carried out in this case, however; although electronic alignment is possible, in principle, a relatively small signal is obtained here with a large offset.

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### Advantages of the Invention

As a refinement of a magnetic sensor system of the type described initially, the magnetic sensor system according to the present invention has two sensor elements in a gradiometer system, each of which is assigned to one of two permanent magnets  
25 having a predetermined separation. In terms of their dimensions, separation and positions relative to the sensor elements, the permanent magnets are located such that the offset of the output signal of the sensor elements is minimized in the gradiometer system.

With the present invention, therefore, the design of a magnetic circuit that produces a working field for a sensor that operates using the gradiometer principle, i.e., by detecting a field gradient, is optimized and therefore enables offset-free operation of the sensor when the magnetic field is varied by mobile transmitter elements, in particular toothed wheels. To this end, the magnetic circuit was created using two individual magnets, the fields of which overlap such that the "in-plane" components of the resultant magnetic field at the gradiometer positions are reduced to the extent that they vary around the zero position due to the influence of the passive transmitter elements. As a result, very small signals can be detected without offset.

This is advantageous, in particular, with highly sensitive magnetoresistive XMR sensors that are designed to cover a large working range, i.e., very large to very small field strengths, without any offset correction, if possible.

With an advantageous embodiment, homogenization plates are located between the sensor elements and the permanent magnets. The field is therefore homogenized in the plane of the sensor elements, and the level of positioning accuracy required of the sensor elements relative to the pair of magnets for offset-free operation is reduced.

It is also advantageous when, according to a further embodiment, the magnetization of each of the permanent magnets is rotated by a specified angle  $\alpha$  relative to their longitudinal direction facing the sensor elements.

Due to this pre-magnetization resulting from the tilted position of the field, the sensor elements are located in a magnetic field in which the sensitivity is a maximum due to a "bias" field. An arrangement of the homogenization plates mentioned above is also advantageously possible in this case.

Particularly advantageously, the present invention can be used with a magnetic sensor system for detecting the angle of rotation of a wheel serving as a transmitter element, the wheel, e.g., a steel wheel, being provided, on its circumference, with teeth for influencing the magnetic field in the region of the magnetic sensor system. Applications in an automobile, in particular, include use as a rotational speed sensor on the wheel or crankshaft, a phase sensor on the camshaft, a rotational speed sensor in the

transmission or as any other type of linear displacement, angular or proximity sensor with which changes in the magnetic field are induced by mobile metallic elements.

### Drawing

5 Exemplary embodiments of the present invention are explained with reference to the drawing.

Figure 1 Shows a schematic illustration of a magnetic sensor system with two permanent magnets, each of which is diametrically opposed to a magnetoresistive sensor element in a gradiometer system,

10 Figure 2 Shows a system that is refined relative to Figure 1, with homogenization plates,

Figure 3 Shows an exemplary embodiment of a magnetic sensor system with two permanent magnets which, in contrast to Figure 1, have a magnetic field positioned at an angle,

15 Figure 4 Shows an exemplary embodiment according to Figure 3 with homogenization plates according to Figure 2,

Figure 5 Shows a view of a magnetic sensor system for a transmitter wheel provided with steel teeth, and

20 Figure 6 Shows a diagram of the course of the magnetic field as a function of the position of a tooth or a tooth space on a transmitter wheel according to Figure 5.

### Detailed Description of the Exemplary Embodiments

Figure 1 shows a schematic illustration of a magnetic sensor system 1 that includes two  
25 permanent magnets 2 and 3, the respective magnetic fields  $B$  of which are oriented with

lines of flux shown in this illustration in the direction toward a sensor 4. In this case, sensor 4 is designed as an XMR sensor and has two magnetoresistive sensor elements 5 and 6. Sensor elements 5 and 6 are shown in a gradiometer system with gradiometer separation GM; they detect the changes in the particular field gradient caused, e.g., by a metallic transmitter element, e.g., a toothed wheel shown in Figure 5, that passes by magnetic sensor system 1.

The optimum working point of sensor 4 is adjusted via distance a between magnets 2 and 3 and can be adapted to the gradiometer separation GM of sensor elements 5 and 6. Furthermore, the courses of the lines of flux depend on the dimensions h, b and t of permanent magnets 2 and 3. Given a fixed gradiometer separation GM, e.g., 2.5 mm, the size, material and arrangement, for example, of permanent magnets 2 and 3 can be determined in this case such that sensor 4 functions in an offset-free manner and can therefore detect the smallest possible signals in order to obtain the greatest possible distance away from a transmitter element.

In the absence of a transmitter element, e.g., a toothed wheel, that is moved past externally, the magnetic lines of flux of magnetic sensor system 1 extend such that a small "in-plane" component toward the outside exists at the location of sensor elements 5 and 6. The use, e.g., of a mobile toothed wheel, causes the magnetic field to vary, the "in-plane" components being modulated around the zero position, so that an offset-free signal is produced by the gradiometer system.

An exemplary embodiment is shown in Figure 2, with which, in contrast to the exemplary embodiment in Figure 1, a homogenization plate 7 is provided between the surfaces of permanent magnets 2 and 3 and sensor 4. With this exemplary embodiment, the field is homogenized in the plane of sensor 4 using homogenization plate 7, therefore reducing the level of positioning accuracy required of sensor 4 relative to the pair of magnets 2, 4 to ensure offset-free operation.

With some of the exemplary embodiments that include magnetoresistive XMR sensor elements 5 and 6 described above, the sensor elements require constant pre-magnetization. As a result of this pre-magnetization, sensor elements 5 and 6 are

located in a magnetic field in which the sensitivity is a maximum. This "bias" field is realized with the exemplary embodiments shown in Figures 3 and 4.

As shown in Figures 3 and 4, this is realized by rotating magnetization B in permanent magnets 2 and 3 by angle  $\alpha$ . In this case, therefore, as described above, two design variations without (Figure 3) and with improved adjustment using a homogenization plate 7 (Figure 4) are realized.

A section of a model is shown in Figure 5, with which magnetic sensor system 1 according to the present invention, e.g., according to Figure 1, is used in combination with a transmitter wheel 8 equipped with teeth 9. A measured result is shown in a diagram in Figure 6 as an example. The "in-plane" component of magnetic field Bx is plotted against the gradiometer position relative to the center of sensor 4, for a tooth 9 (graph 10) and a tooth space (graph 11).

Given a specified test set-up with a gradiometer separation GM of 2.5 mm, it is clear in this case that the course of magnetic field Bx at sensor element position 1.25 mm is symmetrical about the zero position for the two simulated positions of the transmitter wheel 8 (tooth 9, graph 10) and space (graph 11), i.e., the signal of the respective sensor element 5, 6 is offset-free.